

# Combining diving and reflected waves for velocity and impedance models building by waveform inversion

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Grenoble, 12 December 2014



# Outline

- 1 Seismic imaging and FWI principle
- 2 What can we expect from FWI ?
- 3 Some examples of FWI success
- 4 Considering reflected waves : RFWI
- 5 Joint diving/reflected waves FWI
- 6 Synthetic Example: Valhall Case Study
- 7 Conclusion



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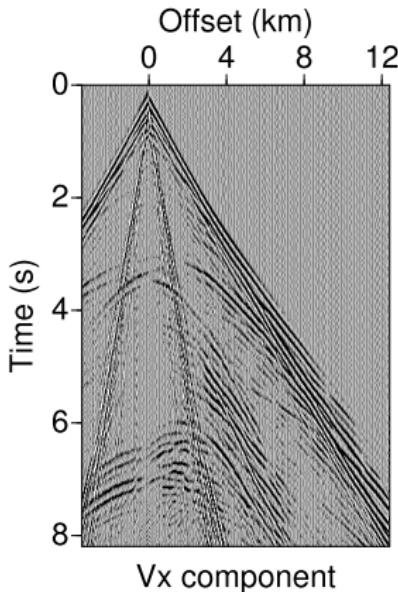
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# Seismic imaging of the Earth

- Quantitative tomography : reconstruction of Earth subsurface properties from remote measurements of seismic waves

$$\frac{\partial U}{\partial t} + \Lambda \frac{\partial U}{\partial x_i} = F_0$$



# Seismic methods : which data ?

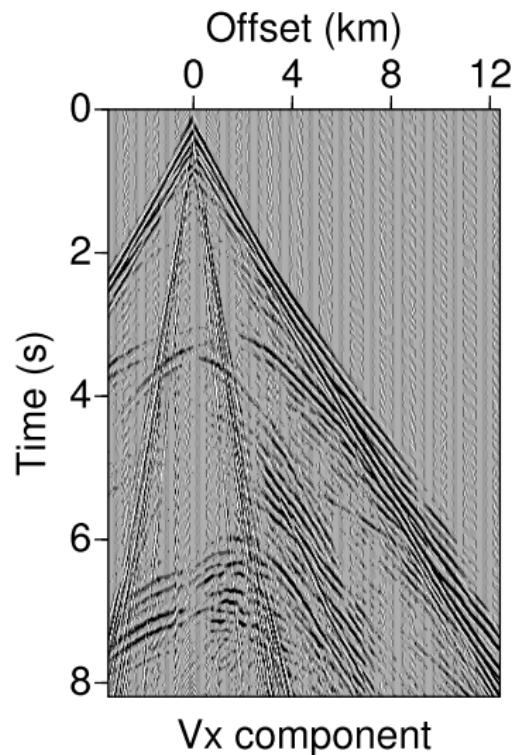
## Different observables from data

- First arrival time tomography
- Reflection tomography
- Migration of reflected/scattered waves
- Refraction tomography
- Surface wave dispersion
- Amplitude analysis (AVO)
- ...

→ All limited information

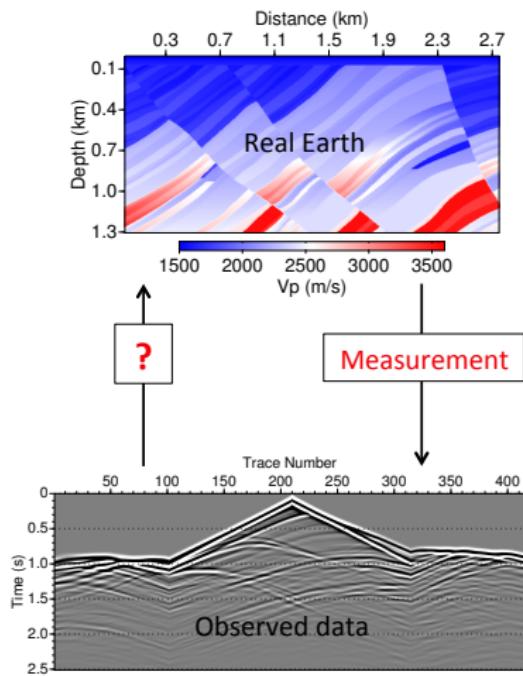
## Full Waveform Inversion (FWI)

- traveltime and amplitude of all arrivals

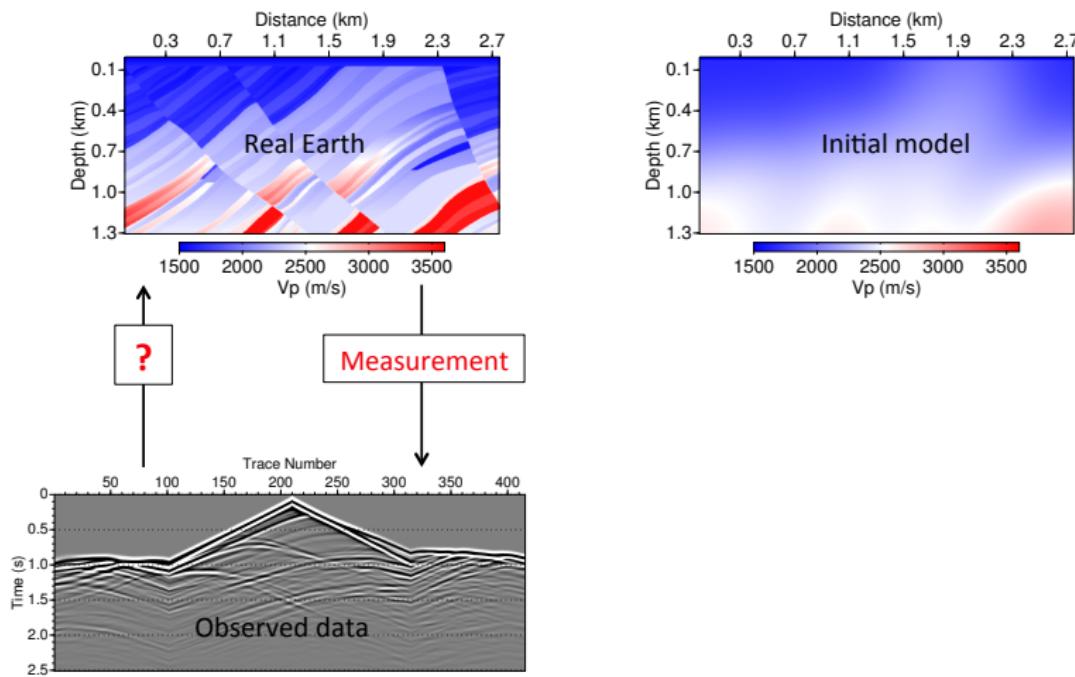


$V_x$  component

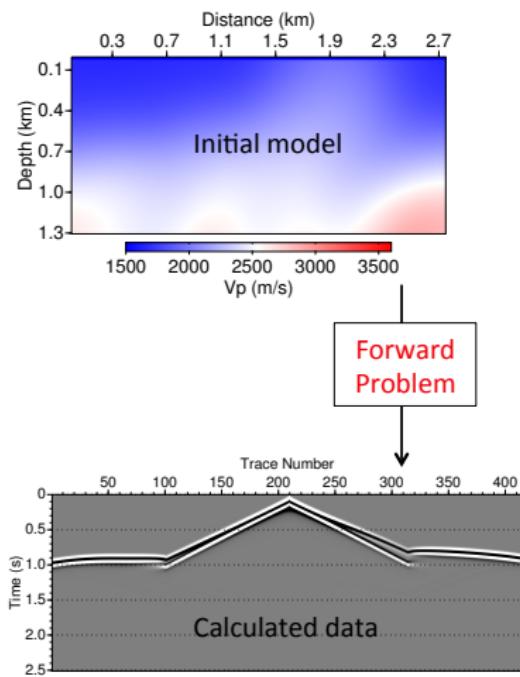
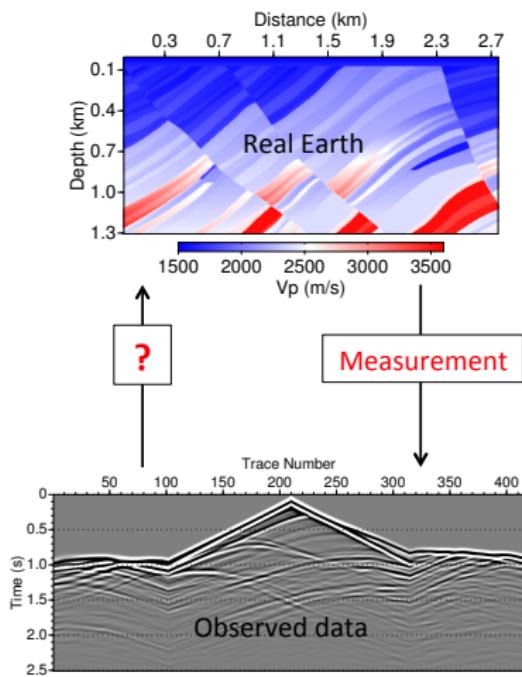
# Full waveform inversion : principle



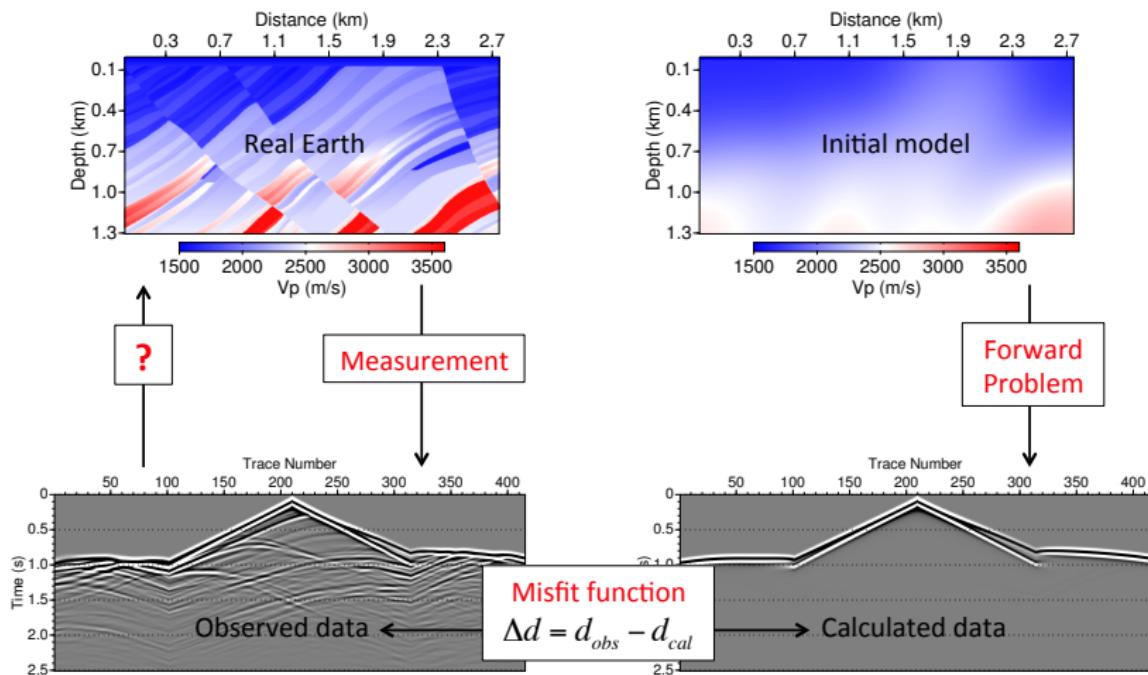
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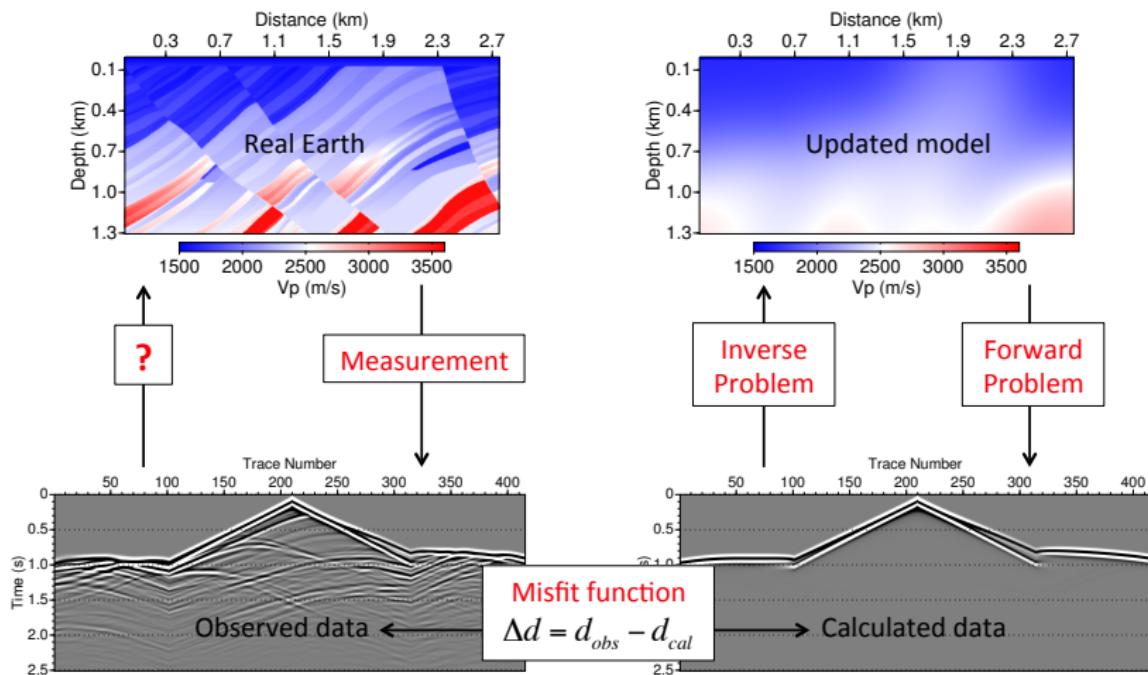
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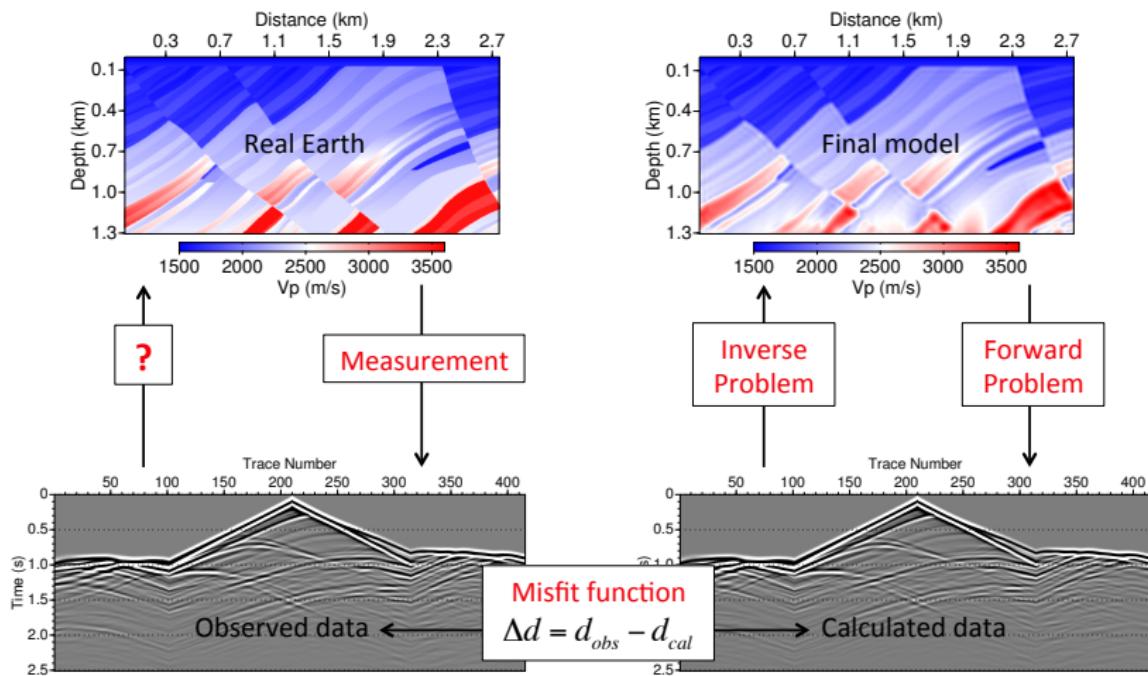
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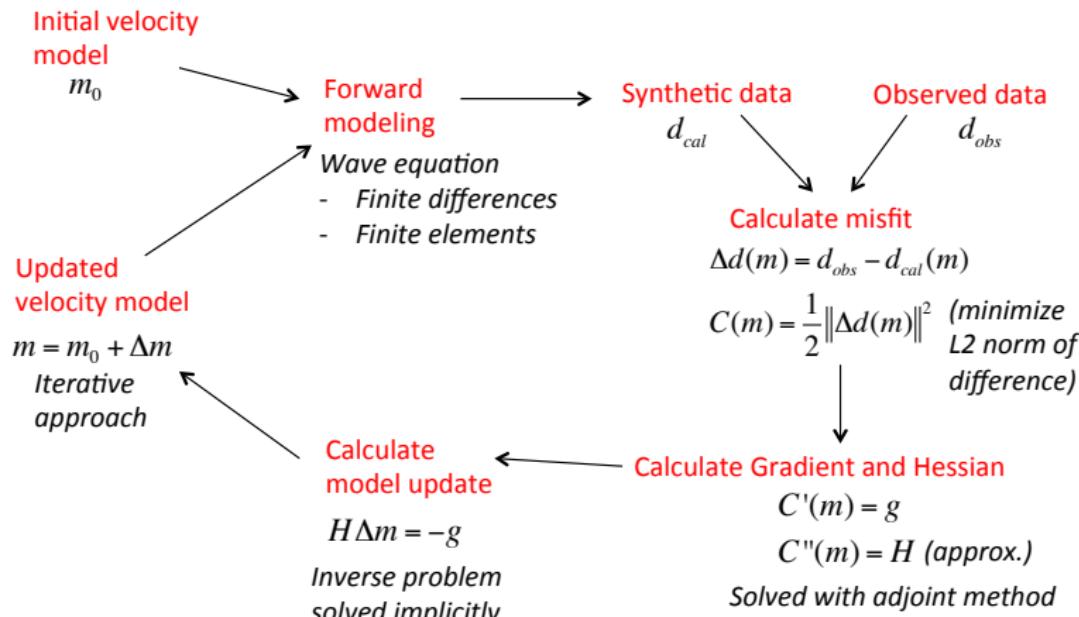
# Full waveform inversion : principle



# Full waveform inversion : principle



# Full waveform inversion : workflow



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## FWI formulation

- FWI : data-fitting procedure which aims to use all the waveforms (Lailly, 1983; Tarantola, 1984; Pratt and Worthington, 1990; Virieux and Operto, 2009)
- Classical FWI misfit function

$$C_{classical} = \sum_{src, rec} \frac{1}{2} \|d_{obs}(t) - d_{pred}(t, m)\|^2 \quad (1)$$

- Lagrangian formulation with adjoint state technique to derive the gradient direction

$$\begin{aligned} L &= \sum_{src, rec} \frac{1}{2} \|d_{obs}(t) - d_{pred}(t)\|^2 + \langle \lambda_1(t) | d_{pred}(t) - R u(t, \mathbf{x}) \rangle_{src, rec, T} \\ &+ \langle \lambda_2(t, \mathbf{x}) | A(m) u(t, \mathbf{x}) - s(t, \mathbf{x}) \rangle_{src, T} \end{aligned} \quad (2)$$

giving

$$A(m) u(t, \mathbf{x}) = s(t, \mathbf{x}) \rightarrow \text{state equation with initial condition}$$

$$A(m)^\dagger \lambda(t, \mathbf{x}) = \sum_{rec} (d_{obs}(t) - d_{pred}(t)) \rightarrow \text{adjoint equation with final condition}$$

leading to the gradient expression (used to predict the descent direction)

$$G_{classical_i} = \sum_{src, rec} u(t, \mathbf{x}) \frac{\partial A(m)^\dagger}{\partial m_i} \lambda(t, \mathbf{x}) \quad (3)$$



# FWI formulation

$$C_{classical} = \sum_{src, rec} \frac{1}{2} \|d_{obs}(t) - d_{pred}(t, m)\|^2 \quad G_{classical_i} = \sum_{src, rec} u(t, \mathbf{x}) \frac{\partial A(m)^\dagger}{\partial m_i} \lambda(t, \mathbf{x})$$



# FWI formulation

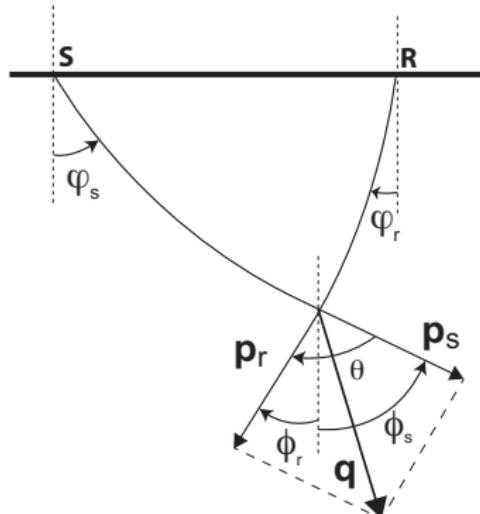
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## FWI intrinsic resolution

- in short, the model update can be seen as the zero-lag cross-correlation

$$G_{\text{classical}} = u \star \lambda \quad (4)$$



- FWI relies on the diffraction tomography principle (Devaney, 1982; Wu and Toksoz, 1987), the updated wavenumber is

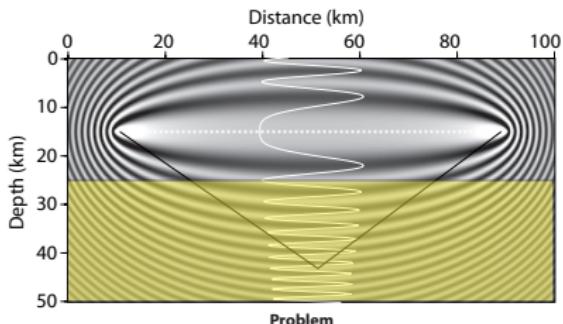
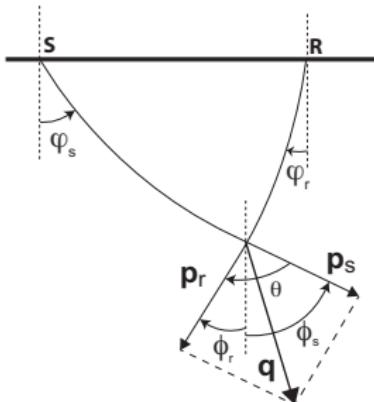


$$\vec{k} = \frac{2\omega}{c_0} \cos\left(\frac{\theta}{2}\right) \frac{\vec{q}}{|\vec{q}|}, \quad (5)$$

# FWI resolution in practice (and associated issues)

$$\vec{k} = \frac{2\omega}{c_0} \cos\left(\frac{\theta}{2}\right) \frac{\vec{q}}{|\vec{q}|},$$

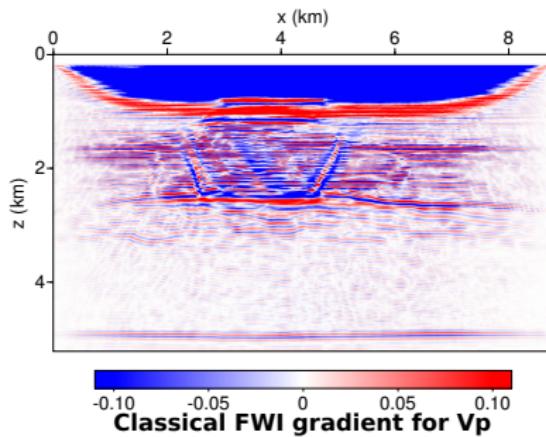
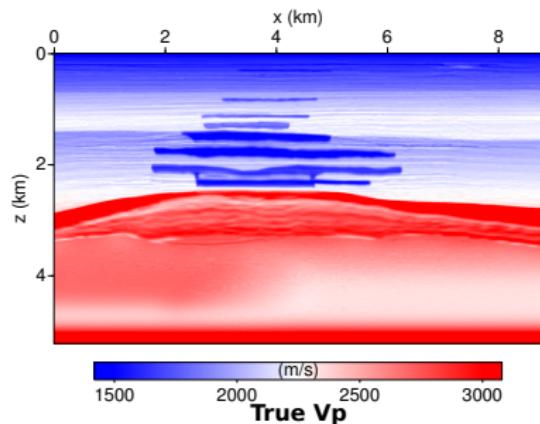
- Shallow targets: A broadband of wavenumbers can be imaged thanks to the broad coverage of scattering angles  $\theta$  provided by transmitted and reflected waves.
- Deep targets: illuminated by short-spread reflections only, leading to high-wavenumber imaging only.  
→ lack of low-wavenumbers if very-low frequencies not available (often the case in practice)



# FWI resolution in practice (and associated issues)

Example of FWI gradient on realistic synthetic case

- Not enough low-frequencies
- limited offset-range : 6 km



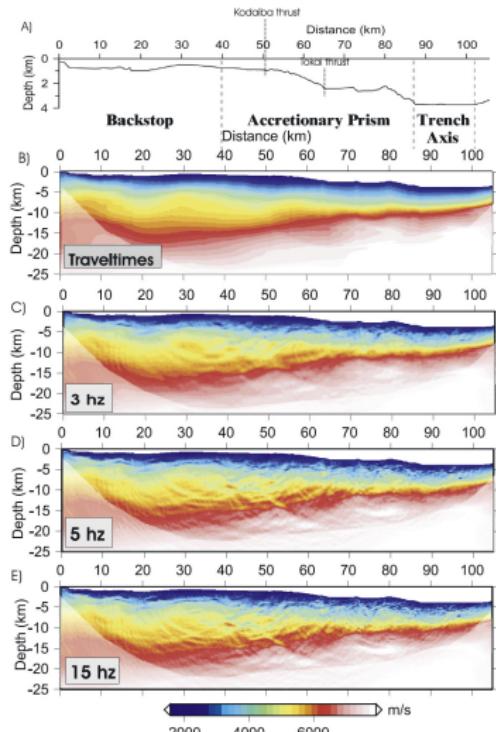
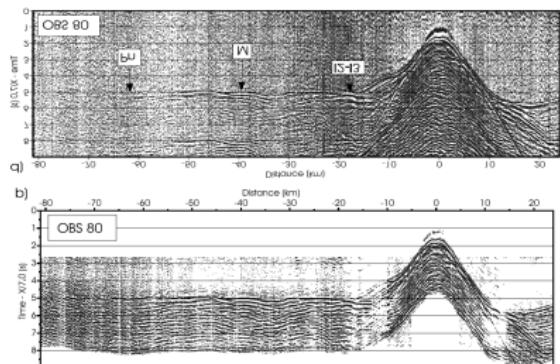
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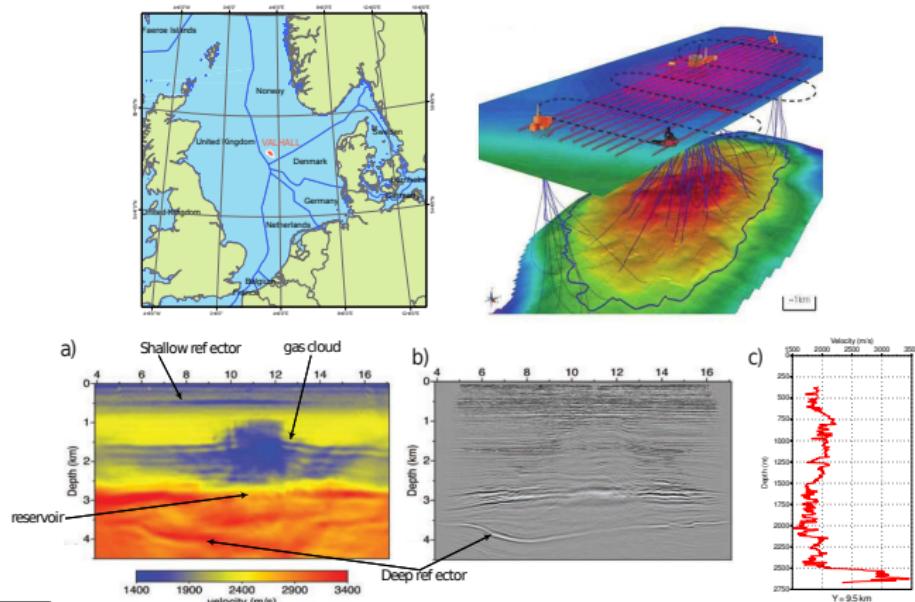
# 2D Imaging of the Nankai trough

- One of the early successfull application on real data, by Operto et al. (2006)



# 3D FWI : OBC Valhall application

- Valhall field : off-shore shallow-water in the North Sea. Over-pressured, under-saturated, Upper Cretaceous chalk reservoir (exploited since 1982)
- Shale at shallow depth : strong imprint of anisotropy in the seismic data
- 3D seismic :  $\approx 50000$  shots, 2414 permanent 4C sensors on the sea bed (OBC)

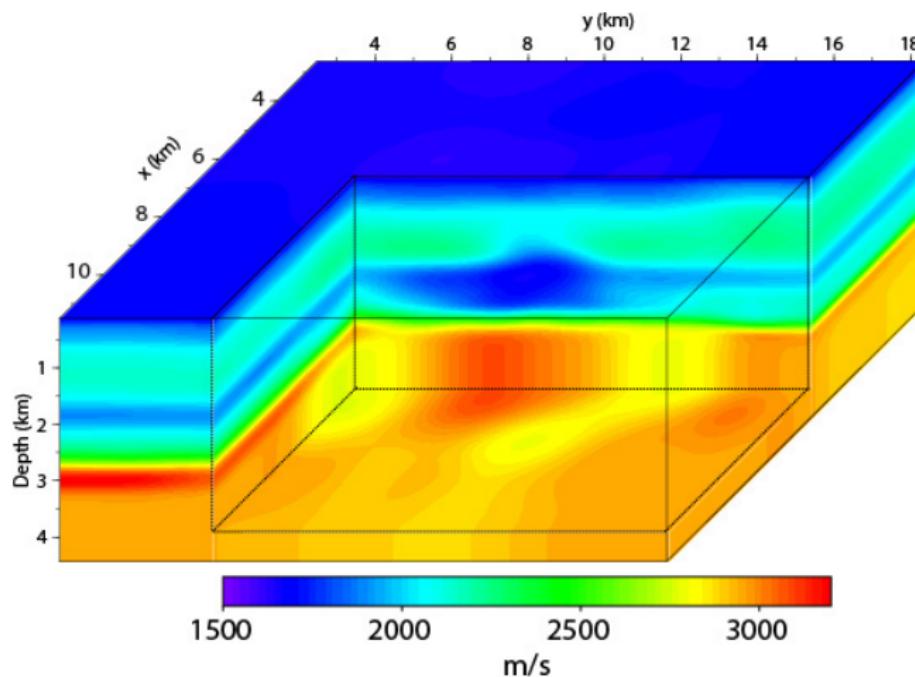


3D Acoustic isotropic FWI by Sirgue et al. (2010)

# 3D FWI : OBC Valhall application

Etienne et al. (2012); Hu et al. (2012)

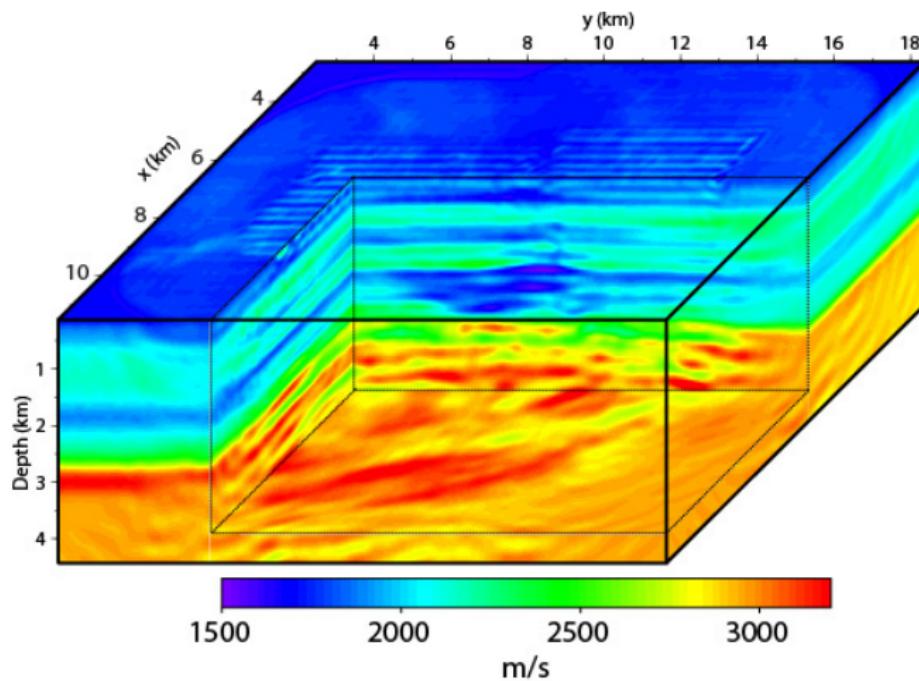
Starting model from reflection tomography



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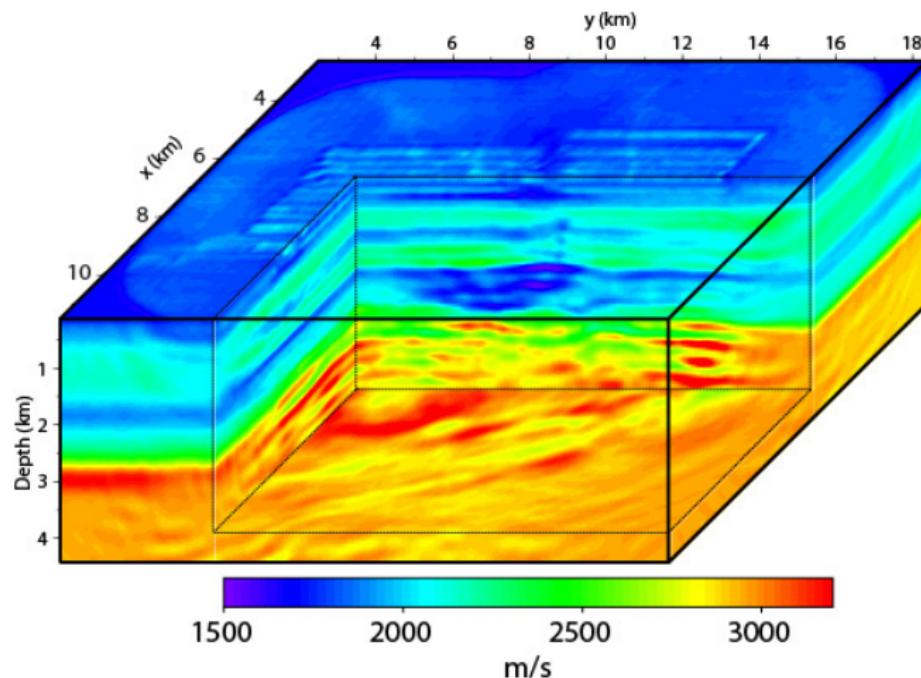
FWI : [3.5,4] Hz



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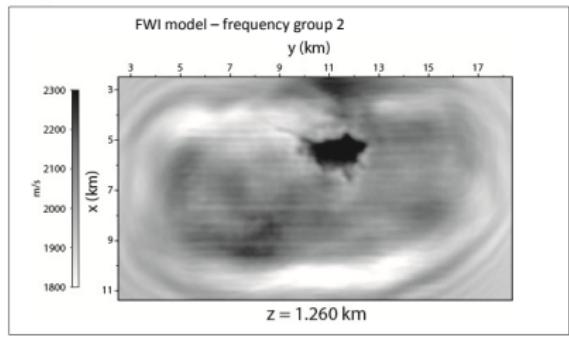
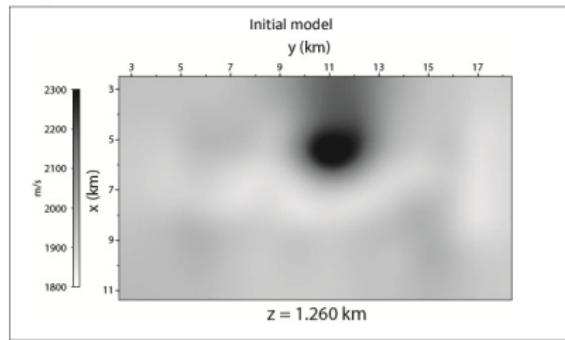
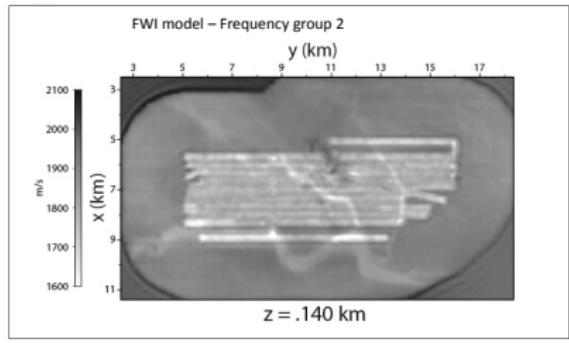
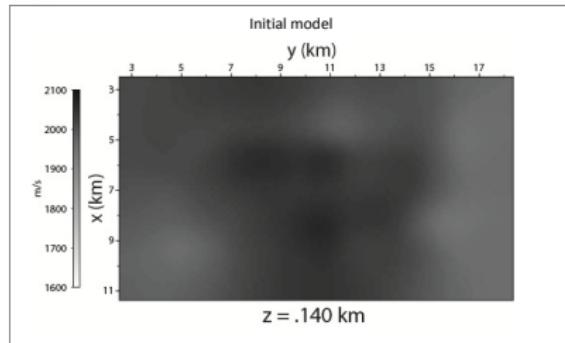
Etienne et al. (2012); Hu et al. (2012)

FWI : [4,5] Hz



# 3D FWI : OBC Valhall application

Etienne et al. (2012); Hu et al. (2012)



## Remarks

- Most of the past and current applications rely on transitted energy
  - Cross-well data in pure transmission
  - Surface data taking benefit of direct, diving and refracted waves
- at depth, a migration-like behavior is observed : only high-wavenumber update  
→ how to take benefit from information coming from reflection energy



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## Velocity model building by reflected waves-based FWI

- Reemerging technique (Xu et al., 2012; Brossier et al., 2014) coming from Migration-Based Traveltime Tomography (Chavent et al., 1994)
- Initial assumption : scale separation between  $m_0, \delta m$  and alternate update
  - Low-wavenumber background velocity model  $m_0$  : RFWI
  - High-wavenumber perturbation model  $\delta m$  : migration or impedance FWI



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- Reflected-wave only misfit function (required to mute direct/diving waves)

$$C_{RFWI} = \frac{1}{2} \| d_{obs}^{refl} - d_{pred}^{refl}(m_0, \delta m) \|^2 \quad (6)$$



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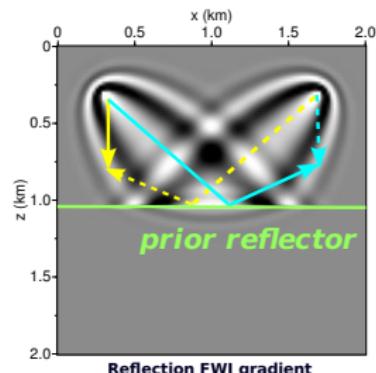
$$C_{RFWI} = \frac{1}{2} \| d_{obs}^{refl} - d_{pred}^{refl}(m_0, \delta m) \|^2 \quad (6)$$

Gradient for  $m_0$ :

$$G_{RFWI} = u_0 \star \delta\lambda + \delta u \star \lambda_0 \quad (7)$$

where

$\left\{ \begin{array}{l} u_0: \text{background part of incident field}, \\ \delta\lambda: \text{scattered part of adjoint field}, \\ \delta u: \text{scattered part of incident field}, \\ \lambda_0: \text{background part of adjoint field} \end{array} \right.$



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# Velocity model building by reflected waves-based FWI

- RFWI focuses on reflected waves only, discarding the low-wavenumber information carried out by transmitted waves.
- Nowadays, very long-offset and wide azimuth acquisitions are well designed, providing the possibility to image the subsurface by including diving waves and postcritical reflections.

→ need to combine diving waves and reflected waves



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  - Workflow
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## Sum of the Two ?

- Inverting all types of waves, still considering explicitly the reflectivity.

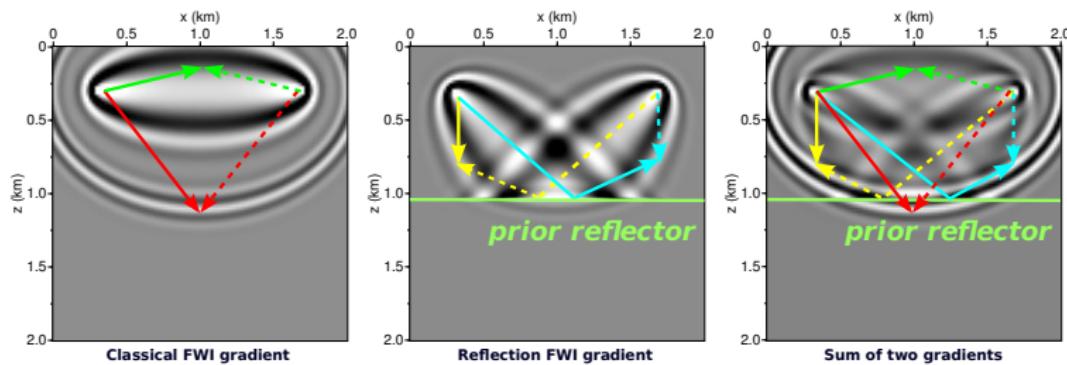
$$C_{FWIwithReflectivity} = \frac{1}{2} \| d_{obs}^{div} - d_{pred}^{div}(m_0) + d_{obs}^{refl} - d_{pred}^{refl}(m_0, \delta m) \|^2 \quad (8)$$



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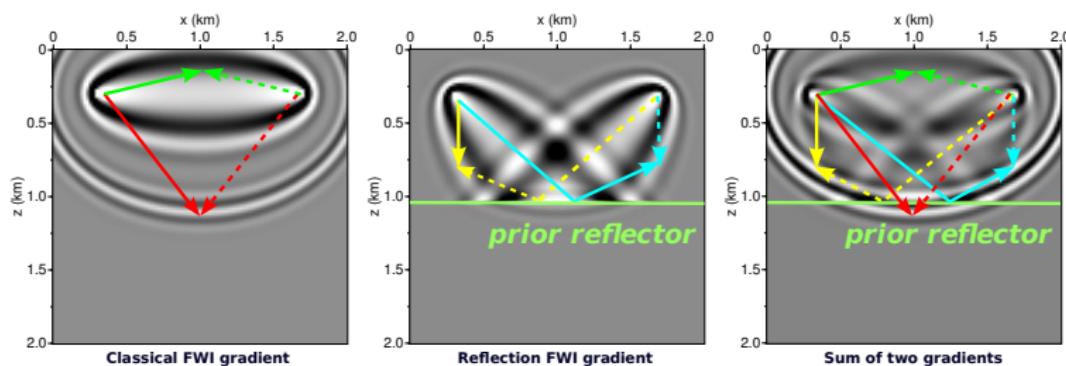
- Problem : The **1st-order isochrones** generated by reflected waves are also injected into the gradient, which damage our low-wavenumber macromodel building.



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- Problem : The **1st-order isochrones** generated by reflected waves are also injected into the gradient, which damage our low-wavenumber macromodel building.  
→ need for a smarter combination !



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# Formalism of the Joint FWI

Zhou et al. (2014)

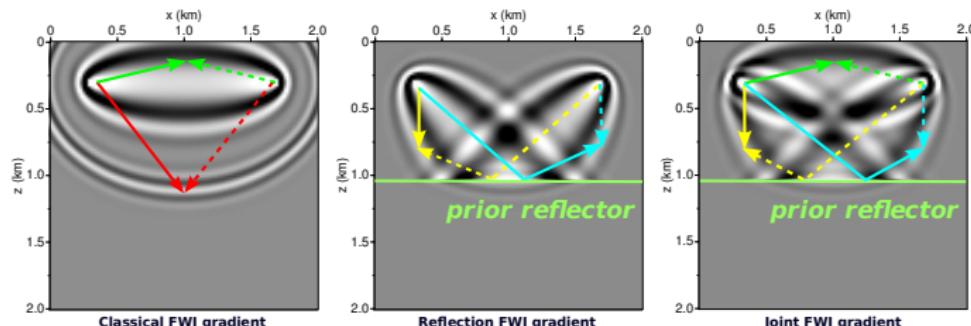
- Misfit function (explicit split between transmitted and reflected energy):

$$C_{JointFWI} = \frac{1}{2} \|W^d \left( d_{obs}^{div} - d_{pred}^{div}(m_0) \right)\|^2 + \frac{1}{2} \|W^r \left( d_{obs}^{refl} - d_{pred}^{refl}(m_0, \delta m) \right)\|^2 \quad (9)$$

where  $W^d$ ,  $W^r$  are weighting operators for diving and reflected waves, respectively.

- Gradient:

$$G_{JointFWI} = u_0 \star \lambda_0^d + u_0 \star \delta \lambda^r + \delta u \star \lambda_0^r + \delta u \star \delta \lambda^r \quad (10)$$



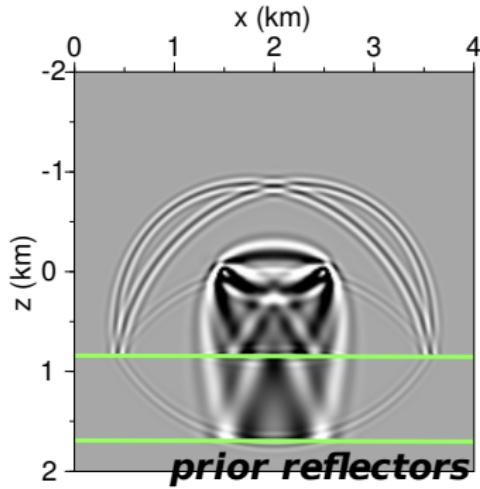
→ low-wavenumber components only thanks to explicit separation



## What happens in a 2 reflectors case ?

$$G_{JointFWI} = u_0 \star \lambda_0^d + u_0 \star \delta\lambda^r + \delta u \star \lambda_0^r + \delta u \star \delta\lambda^r \quad (11)$$

- the presence of  $\delta m$  generates multi-scattered waves, leading to unphysical higher-order isochrones  
→ same effects that classical migration edge-artifacts
- stacking over sources and receivers should mitigate their energy
- appropriate parametrization is important



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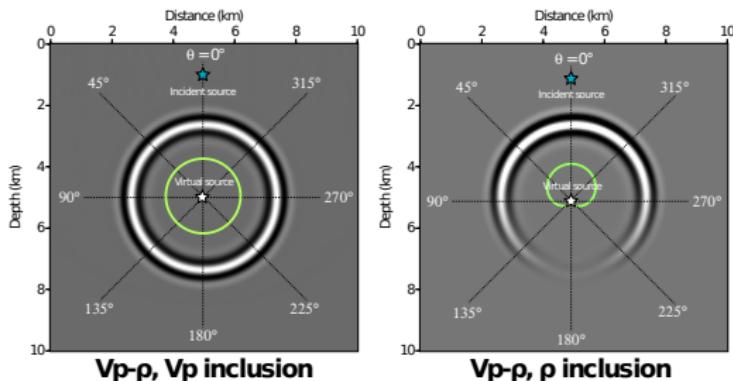
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# Importance of parametrization

## $V_P - \rho$ parameterization:

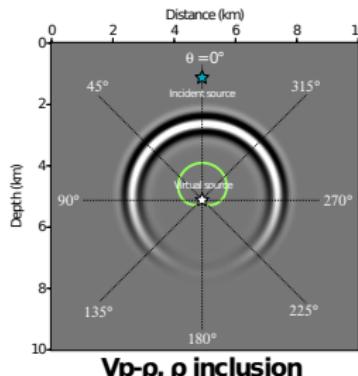
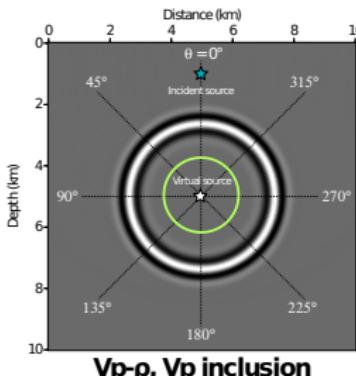
- (Left)  $V_P$ : Isotropic pattern for  $V_P$  diffractor. Scattered wave is equally energetic from short to wide  $\theta$ .
- (Right)  $\rho$ : Scattering at short-to-intermediate  $\theta$ .
- Cross-talks of  $V_P$  and  $\rho$  at short-to-intermediate  $\theta$ .



# Importance of parametrization

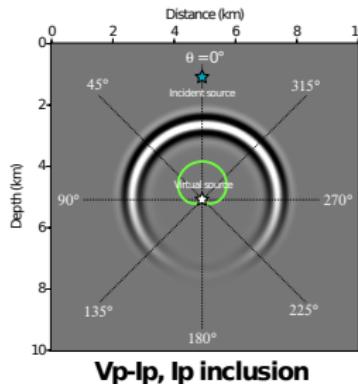
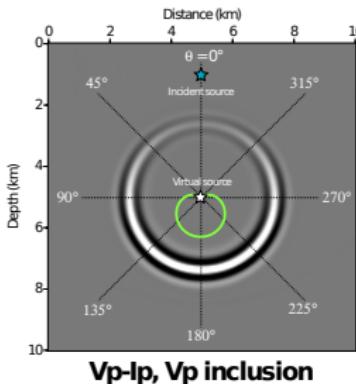
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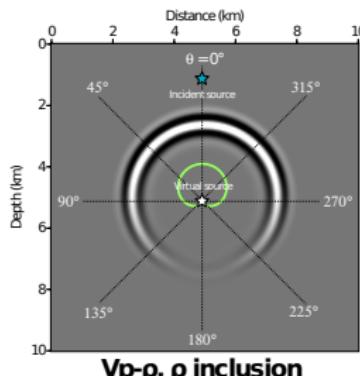
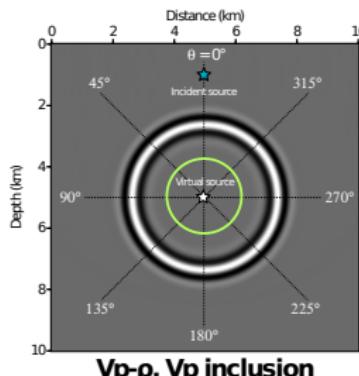
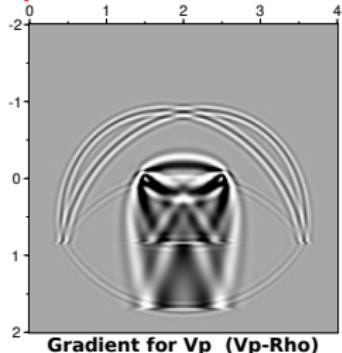
## $V_P - I_P$ parameterization:

- (Left)  $V_P$ : Scattering at intermediate-to-wide  $\theta$ .
- (Right)  $I_P$ : Scattering at short-to-intermediate  $\theta$ .
- Less cross-talks and keeping low wavenumbers in  $V_P$ .

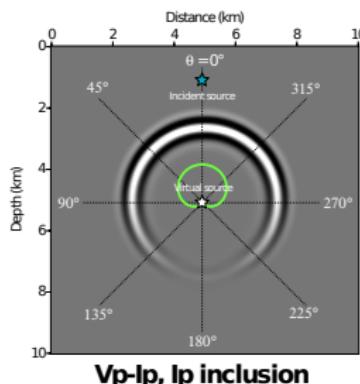
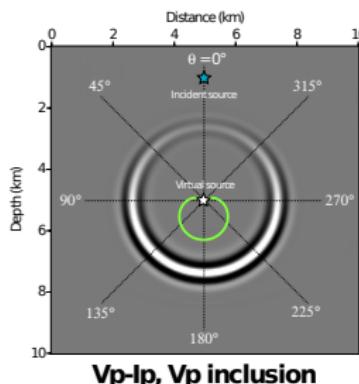
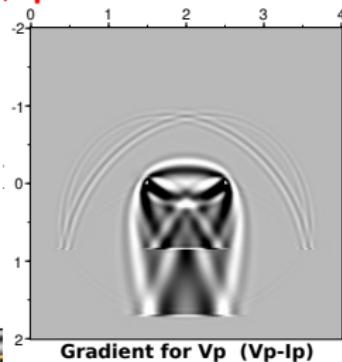


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$V_P - \rho$  parameterization:



$V_P - I_P$  parameterization:



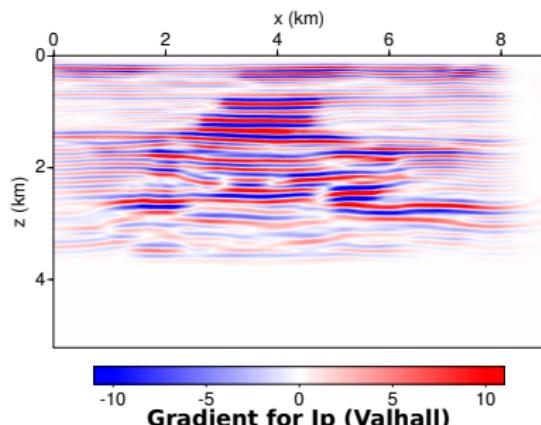
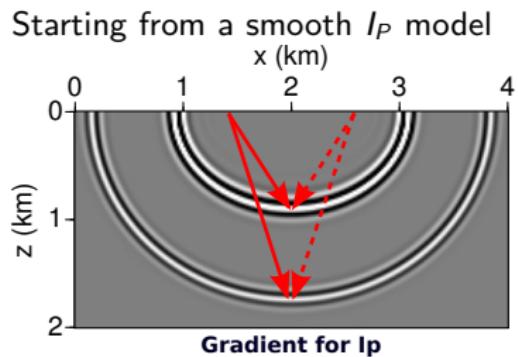
# Perturbation imaging by impedance Inversion

- The high-wavenumber perturbation  $\delta m$  is built through  $I_P$  inversion in FWI.
- Misfit function:

$$C_{I_P} = \frac{1}{2} \| W^r \left( d_{obs}^{refl} - d_{pred}^{refl}(m_0, \delta m) \right) \|^2 \quad (12)$$

- Gradient:

$$G_{I_P} = u_0 \star \lambda_0^r \quad (13)$$



# Outline

- 1 Seismic imaging and FWI principle
- 2 What can we expect from FWI ?
- 3 Some examples of FWI success
- 4 Considering reflected waves : RFWI
- 5 Joint diving/reflected waves FWI
  - Formalism of the Joint FWI
  - On the Importance of Subsurface Parametrization
  - Workflow
- 6 Synthetic Example: Valhall Case Study
- 7 Conclusion



# Algorithm for the whole Workflow

Smooth  $V_P$  and  $I_P$  initials

**repeat**

**USE** initial (or updated)  $V_p$

**USE** initial  $I_p$ , NO reflectivity

**DO**  $I_p$  inversion

**GET** reflectivity in  $I_p$   
(high-wavenumber content)

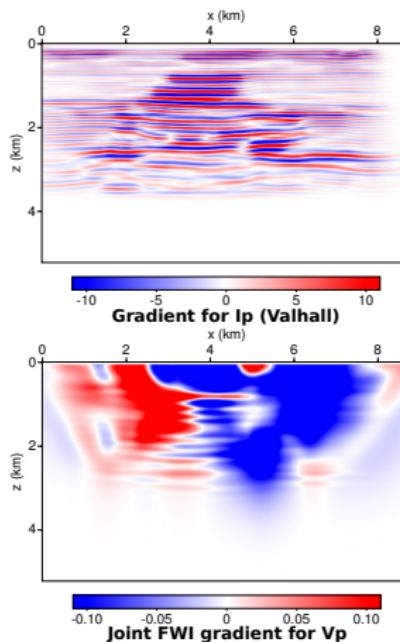
**USE** initial (or updated)  $V_p$

**USE**  $I_p$  with reflectivity

**DO**  $V_p$  inversion

**GET** updated  $V_p$   
(low-wavenumber content)

**until** convergence

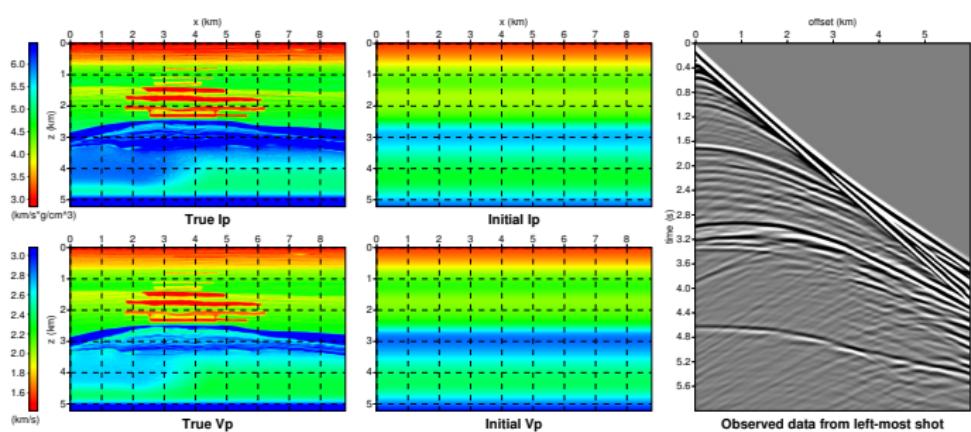


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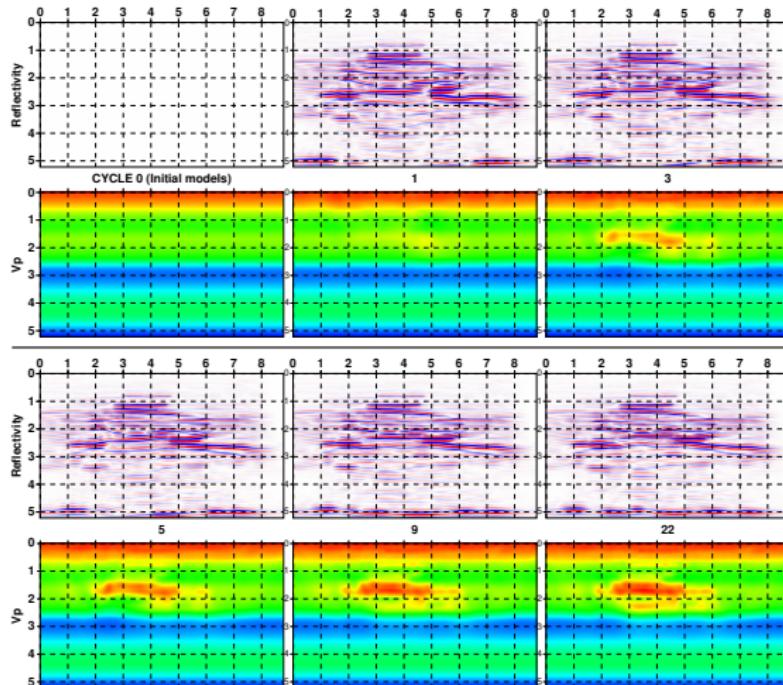


# Models and Configurations

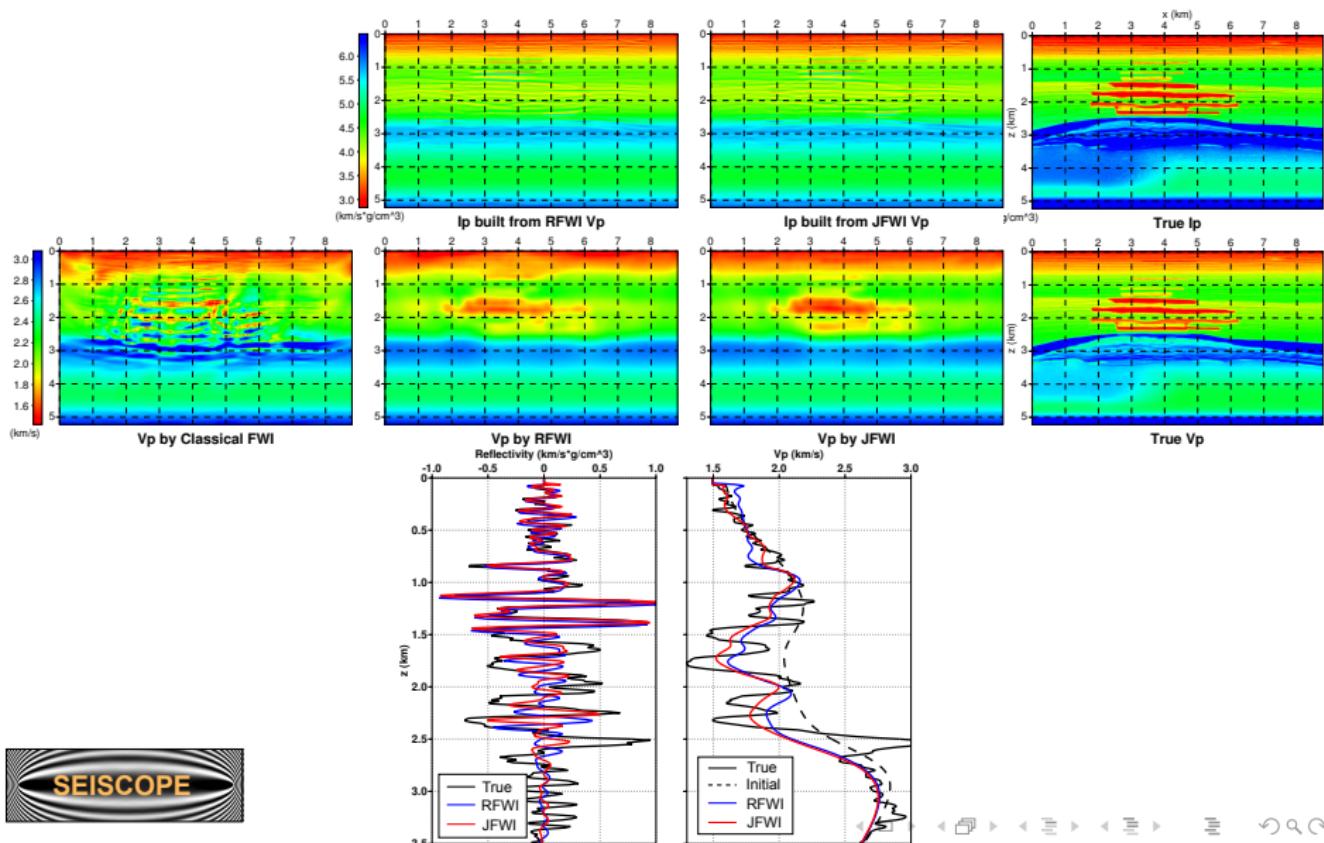


# Results during the iterative process

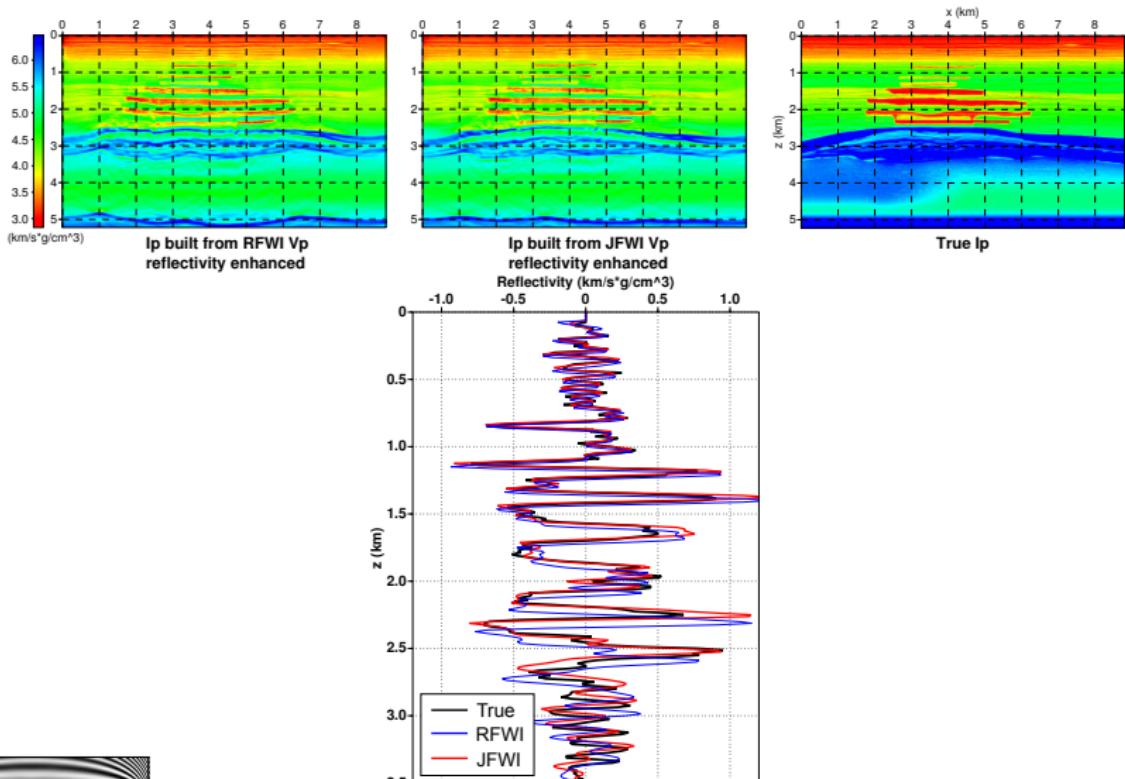
Alternate update of reflectivity (through impedance) and velocity



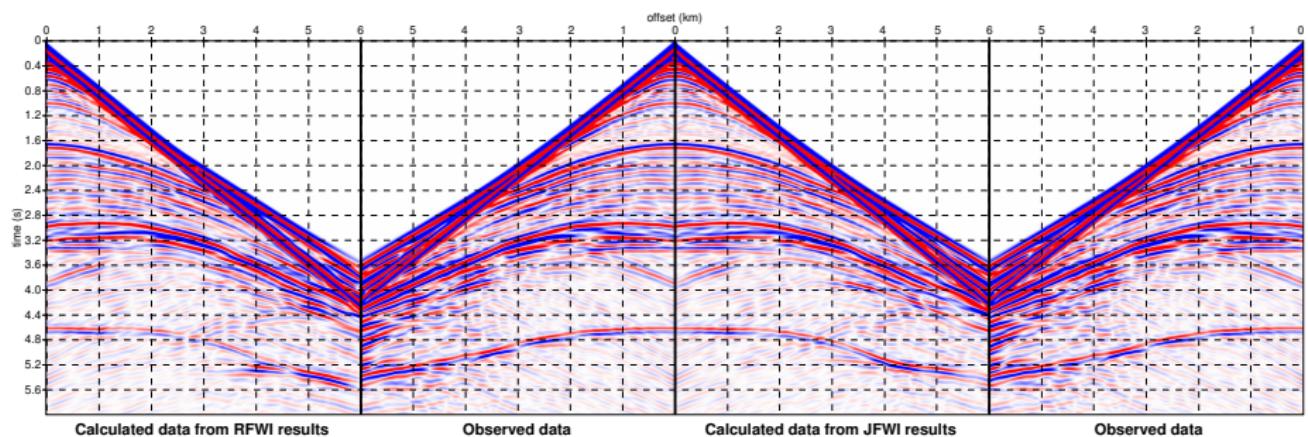
# Final results and comparison



# Final Impedance estimation : benefit of JFWI



# Data fit



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- 1 Seismic imaging and FWI principle
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# Conclusion

- Despite a number of success to real data, classical FWI formulation is unable to use reflected waves to update the full wavenumber spectrum : problem at depth when lack of diving-wave coverage.
- Using an explicit wavenumber separation of the model representation and alternate updates
  - Reflected-wave FWI allows to take benefit of reflected wave information for velocity model building, but discard a large part of recorded energy
  - Our joint FWI scheme allows to fully benefit from both the diving waves and reflected waves information
- RFWI and JFWI rely on an explicit scale separation.  $V_P - I_P$  parametrization is the most suitable choice to honor this scale separation.
- Applications on the synthetic Valhall shows the benefit of the JFWI scheme over RFWI.



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